

16-311-Q INTRODUCTION TO ROBOTICS

LECTURE 10A: FEEDBACK-BASED CONTROL 2A

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TO BE DONE ...

Stability properties of linear systems Linearization of previous control systems Stability domain for feedback-based gains Other types of controllers?

CONTROLLABILITY OF A DYNAMICAL SYSTEM

Time-invariant dynamical system with *m* control inputs \mathbf{u} $\dot{\mathbf{x}} = f(\mathbf{x}(t), \mathbf{u}(t)), \quad \mathbf{x} \in \mathbb{R}^{n}, \ \mathbf{u} \in \mathbb{R}^{m}$

Control inputs are defined according to a **feedback law**: u(t) = Kx(t), K is an $n \times m$ feedback Gain matrix

Controllability: Any initial state x(0) can be steered to any final state x^1 at a finite time t_1 based on the inputs from the feedback law.

For a robot: All configurations can be achieved in finite time from a given initial configuration. Note: The trajectory between 0 and t₁ is not specified

For linear dynamical systems $f(\mathbf{x}(t), \mathbf{u}(t)) = A\mathbf{x}(t) + B\mathbf{u}(t)$ algebraic criteria for controllability are available:

 $C = [B AB A^2B \cdots A^{n-1}B], \text{ rank}(C) = n (C \text{ has full rank})$

For non-linear dynamical systems, general controllability criteria are not available!

Local (in space and time) notions of controllability are employed

STABILITY OF A DYNAMICAL SYSTEM

Equilibrium: A state x^e of is said to be an *equilibrium state* if and only if $x^e = x(t; x^e, u(t)=0)$ for all $t \ge 0$.

If a trajectory reaches an equilibrium state and if no input is applied the trajectory will stay at the equilibrium state forever (internal system's dynamics doesn't move the system away from the equilibrium point)

For a linear system the zero state is a always an equilibrium state

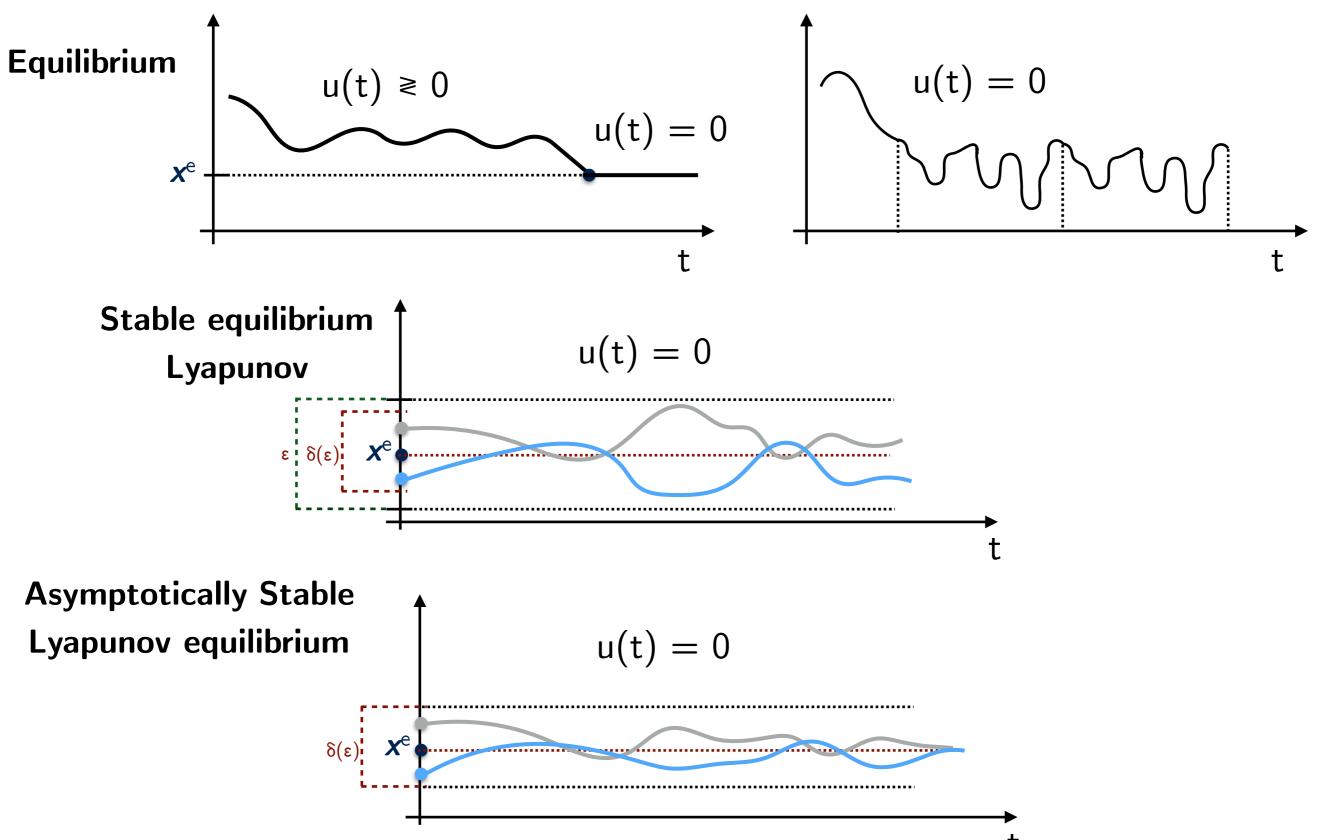
Stable equilibrium: An equilibrium state x^e is said to be *stable* if and onlyif for any positive ε , there exists a positive number $\delta(\varepsilon)$ such that the inequality $||x(0) - x^e|| \le \delta$ Lyapunov stability

implies that $||x(t; x(0), u(t)=0) - x^{e}|| \le \varepsilon$ for all $t \ge 0$.

An equilibrium state x^e is stable if the response following after starting at any initial state x(0) that is sufficiently near to x^e will not move the state far away from x^e .

Asymptotically stable equilibrium: If the equilibrium x^e is Lyapunov-stable and if every motion starting sufficiently near to x^e converges (go back) to x^e as $t \to \infty$.

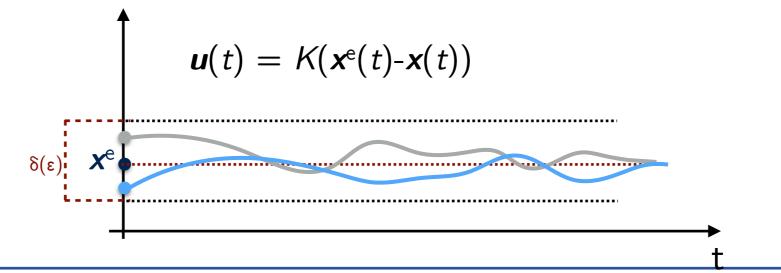
ILLUSTRATION OF STABILITY TYPES



CONTROLLABILITY VS. STABILIZABILITY

Stabilizability: The problem of finding a <u>feedback control law</u> so as to make a closed-loop equilibrium point x^e or admissible trajectory $x^e(t)$ asymptotically stable.

Stabilizability is very important in practice to be able to cope with real-world disturbances



Stabilizability of Linear dynamic systems:

Controllability implies asymptotic (actually, exponential) stabilizability by a smooth state feedback law. In fact, the controllability condition implies that there exist choices of the constant gain matrix K such that the linear P control

$$\boldsymbol{u}(t) = K(\boldsymbol{x}^{e}(t) - \boldsymbol{x}(t))$$

makes $\mathbf{x}^{e}(t)$ asymptotically stable

Linear systems: Controllability → Stabilizability Non-Linear systems:

Controllability ? Stabilizability

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LINEAR DYNAMIC SYSTEMS

Given a linear dynamic system in the form of a homogeneous system of ODEs: $\dot{x}(t) = Ax(t)$

• Where will the system state go? \rightarrow Solve the system to find the time-dependent function $\mathbf{x}(t)$ for the evolution of the state variables.

$$\begin{bmatrix} \frac{dx_1}{dt} \\ \frac{dx_2}{dt} \end{bmatrix} = A \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} 4 & 8 \\ 10 & 2 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

The solution function for the state variables is the following, with c_1 and c_2 integration constants depending on the initial point x(0):

$$\begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} c_1 e^{12t} + c_2 4 e^{-6t} \\ c_1 e^{12t} - c_2 5 e^{-6t} \end{bmatrix} = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{12t} + c_2 \begin{bmatrix} 4 \\ -5 \end{bmatrix} e^{-6t}$$

A's eigenvalues $\lambda_1 = 12, \ \lambda_2 = -6$ $r_1 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, r_2 = \begin{bmatrix} 4 \\ -5 \end{bmatrix}$ *A's* eigenvectors

In the general case of a system with n state variables (equations)

$$\mathbf{x}(t) = c_1 \mathbf{r}_1 e^{\lambda_1 t} + c_2 \mathbf{r}_2 e^{\lambda_2 t} + \dots + c_n \mathbf{r}_n e^{\lambda_n t}$$

LINEAR DYNAMIC SYSTEMS

• Where are the equilibrium points? Answering means to first find the **fixed points** (the **attractors**, in general) that correspond to <u>setting to zero the rate of variability</u> <u>of the state variables</u>. In the example, the fixed points are the solutions of:

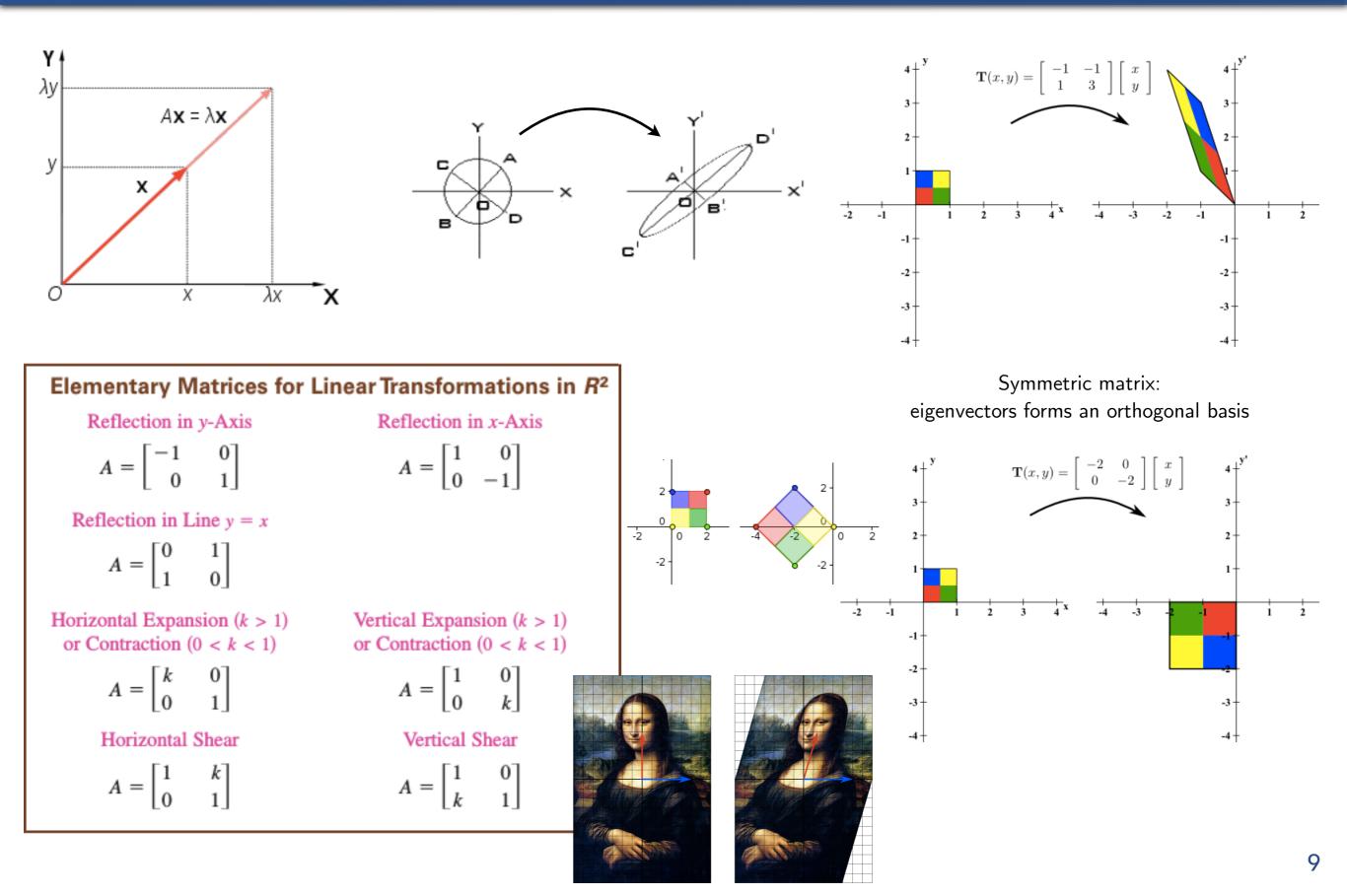
$$\begin{bmatrix} 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 4 & 8 \\ 10 & 2 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

• What will the system do in correspondence of the fixed points? Is the system (asymptotically) *stable*? If we place the system close to a fixed point, or, similarly, we disturb a system at a fixed point, will the system go back to the fixed point, or will it diverge from it? What about the behavior at any other point?

For a **linear system**, a stability analysis for the fixed points can be performed through the calculation of the eigenvalues of the matrix of the coefficients.

The <u>eigenvalues</u> are the solution of the characteristic equation det(A - λ I) = 0, and determine the time evolution of the system along the <u>principal directions of the eigenvectors</u>

RECAP ON EIGENVALUES AND EIGENVECTORS



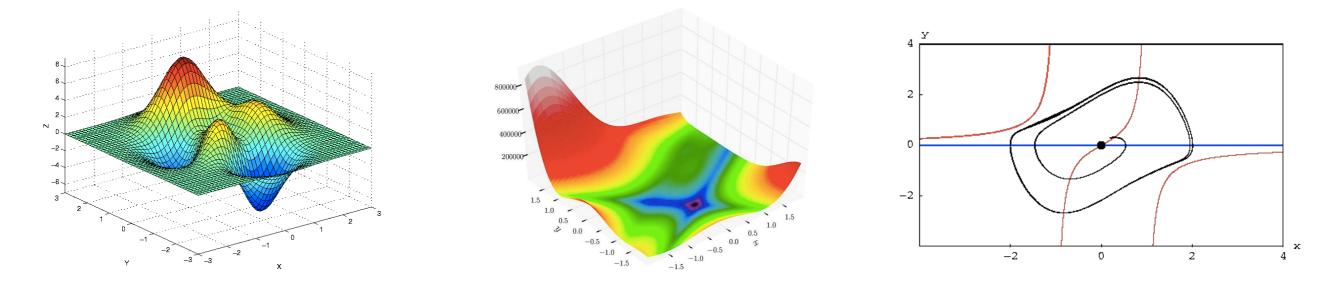
(LINEAR) STABILITY BEHAVIOR VS. EIGENVALUES

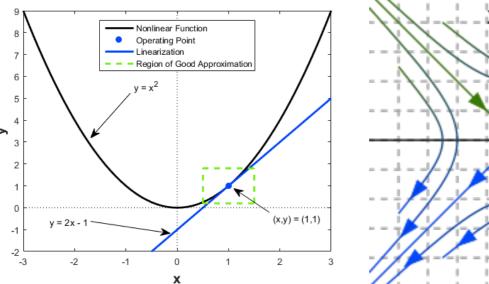
State behavior in the vicinity of a fixed point in relation to its stability based on the eigenvalues (the value of y axis quantifies the distance from the fixed point)

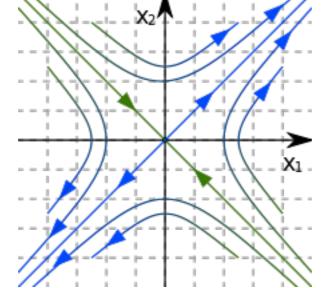
Eigenvalues	Graph	Eigenvalue Type	Stability	Oscillatory Behavior	Notation
All real and negative		All Real and +	Unstable	None	Unstable Node
		All Real and -	Stable	None	Stable Node
		Mixed + & - Real	Unstable	None	Unstable saddle point
All real and one or more are positive	20000	+a + b <i>i</i>	Unstable	Undamped	Unstable spiral
	10000	-a + bi	Stable	Damped	Stable spriral
	5000	0 + bi	Unstable	Undamped	Circle
All real eigenvalues are negative and there are	A0	Repeated values	5 Depends on orthogonality of eigenvectors		
imaginary parts		Negative real part =	-	Complex eigenvalues	Positive real part= unstable
One or more eigenvlaues have a positive real part and there are imaginary parts	5000 -5000 -10 000 -10 000 -20 000	spiral	$\mathbf{\bullet}$. .	spiral
Real parts of the eigenvlaues are zero and there are imaginary parts		Two real negative roots = stable node			Two real positive roots = unstable node
		Real roots of opp. sign = unstable saddle node			

NON-LINEAR DYNAMICAL SYSTEMS?

A *non-linear system can be linearized around a (fixed) point*, and studied with the same methods. The effectiveness of the linearization decreases with the <u>distance</u> from the fixed point itself and with the <u>stability characteristics of the point</u>.







Hartman-Grobman theorem: In a hyperbolic equilibrium point where <u>all eigenvalues have non-</u> <u>zero real parts</u>, the flows of the linearized and nonlinear system are (topologically) equivalent near the equilibrium. In particular, the stability of the nonlinear equilibrium is the same as the stability of the equilibrium of the linearized system.

Hyperbolic point (near the point trajectories resemble hyperbolas) Saddle point

This is what we have derived:

lt's

$$\begin{aligned} v(t) &= \kappa_{\rho}\rho(t) \\ \gamma(t) &= \kappa_{\alpha}\alpha(t) + \kappa_{\beta}\beta(t) \\ \begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} -\cos(\alpha) & 0 \\ \frac{\sin(\alpha)}{\rho} & -1 \\ -\frac{\sin(\alpha)}{\rho} & 0 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix} \\ \dot{\beta} \end{bmatrix} \\ = \begin{bmatrix} -\kappa_{\rho}\rho\cos(\alpha) \\ -\kappa_{\rho}\sin(\alpha) - \kappa_{\alpha}\alpha - \kappa_{\beta}\beta \\ -\kappa_{\rho}\sin(\alpha) \end{bmatrix} \end{aligned}$$

$$\begin{aligned} ?? \text{ Asymptotically stable as long as:} \\ \kappa_{\rho} &> 0, \quad \kappa_{\beta} < 0, \quad \kappa_{\alpha} - \kappa_{\rho} > 0 \\ -\kappa_{\rho}\sin(\alpha) \end{bmatrix}$$
NOT linear in the state $[\rho(t) \alpha(t) \beta(t)]$

Linearization around the fixed point [0 0 0]

LINEARIZATION OF THE CONTROL LAW

$$\begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} -\kappa_{\rho} \cos(\alpha) \\ -\kappa_{\rho} \sin(\alpha) - \kappa_{\alpha} \alpha - \kappa_{\beta} \beta \\ -\kappa_{\rho} \sin(\alpha) \end{bmatrix}$$
 In a small neighborhood of [0 0 0]:

$$\cos(x) = 1, \sin(x) = x$$

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$$\frac{\dot{\rho}}{\alpha} = \begin{bmatrix} -\kappa_{\rho} & 0 & 0 \\ 0 & -(\kappa_{\alpha} - \kappa_{\rho}) & -\kappa_{\beta} \\ 0 & -\kappa_{\rho} & 0 \end{bmatrix} \begin{bmatrix} \rho \\ \alpha \\ \beta \end{bmatrix}$$

$$\frac{\text{Linearization}}{\text{around the fixed point [0 0 0]}}$$

The characteristic polynomial of the coefficient (gain) matrix A is

 $\begin{aligned} & \left(\lambda + K_{\rho}\right) \left(\lambda^{2} + \lambda (K_{\alpha} - K_{\rho}) - K_{\rho} K_{\beta}\right) & \text{ all roots have negative real part (i.e., stability) if } \\ & K_{\rho} > 0, \quad K_{\beta} < 0, \quad K_{\alpha} - K_{\rho} > 0 \end{aligned}$

For **robust pose control**, the following strong stability conditions ensures that the robot does not change direction approaching the goal, implying that conditions on α $K_{\rho} > 0$, $K_{\beta} < 0$, $K_{\alpha} + \frac{5}{3}K_{\beta} - \frac{2}{\pi}K_{\rho} > 0$ If $\alpha(0) \in I_{f} = \left(-\frac{\pi}{2}, \frac{\pi}{2}\right] \Rightarrow \alpha(t) \in I_{f} \forall t$ If $\alpha(0) \in I_{b} = \overline{I}_{f} \Rightarrow \alpha(t) \in I_{b} \forall t$

FUNCTION LINEARIZATION

Linearization requires first-order differenziability. For a scalar function f(x) of one variable, the Taylor series of the 1st order in a point x₀:

$$f(x) = f(x_0) + f'(x_0)(x - x_0) + o(x - x_0)$$

is the same as the equation of the tangent line in x_0 (up to an error of the second order), that is, the derivative defines the linear approximation of the function.

- For a scalar function of multiple variables, the gradient vector ∇f(x) generalizes the notion of derivatives for all variables, and linearization is performed using the same Taylor's series but using the gradient instead of the derivative.
- For a vector function g(x) : ℝⁿ → ℝ^p, the relation still holds, but the gradient vector is substituted by the Jacobian matrix:

$$\boldsymbol{J}(\boldsymbol{x}) = [\nabla g_1(\boldsymbol{x}) \dots \nabla g_p(\boldsymbol{x})]^T = \begin{pmatrix} \frac{\partial g_1}{\partial x_1} & \frac{\partial g_1}{\partial x_2} & \dots & \frac{\partial g_1}{\partial x_n} \\ \frac{\partial g_2}{\partial x_1} & \frac{\partial g_2}{\partial x_2} & \dots & \frac{\partial g_2}{\partial x_n} \\ \dots & \dots & \dots & \dots \\ \frac{\partial g_p}{\partial x_1} & \frac{\partial g_p}{\partial x_2} & \dots & \frac{\partial g_p}{\partial x_n} \end{pmatrix}, \quad \boldsymbol{J}^T(\boldsymbol{x}) = \begin{pmatrix} \frac{\partial g_1}{\partial x_1} & \frac{\partial g_2}{\partial x_1} & \dots & \frac{\partial g_p}{\partial x_1} \\ \frac{\partial g_1}{\partial x_2} & \frac{\partial g_2}{\partial x_2} & \dots & \frac{\partial g_p}{\partial x_2} \\ \dots & \dots & \dots & \dots \\ \frac{\partial g_1}{\partial x_n} & \frac{\partial g_2}{\partial x_n} & \dots & \frac{\partial g_p}{\partial x_n} \end{pmatrix}$$

- A dynamic system of p equations in n state variables can be precisely seen as a vector function, with the Jacobian showing how every variable changes with the variation of another variable derivatives
- The general approach for the linearization of a dynamic system passes through the writing of the Jacobian matrix at the fixed point of interest x_0 , and use of the resulting Jacobian to write the Taylor's series of the first order that linearly approximates the system in x_0 317